



## Fine grains ceramics of PIN–PT, PIN–PMN–PT and PMN–PT systems: Drift of the dielectric constant under high electric field

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### 8 Abstract

Lead-based ferroelectric ceramics with  $(1-x)\text{Pb}(\text{B}_1\text{B}_2)\text{O}_3-x\text{PbTiO}_3$  formula have emerged as a group of promising materials for various applications like ultrasonic sonars or medical imaging transducers [Y.H. Chen, K. Uchino, J. Appl. Phys. (2001) 3928–3933].  $(1-x)\text{PMN}-x\text{PT}$ ,  $(1-x)\text{PIN}-x\text{PT}$  and ternary solutions  $x\text{PIN}-y\text{PMN}-z\text{PT}$  ceramics are synthesised using the solid state reaction method [Y. Hosono, Y. Yamashita, H. Sakamoto, N. Ichinose, Jpn. J. Appl. Phys. 42 (2003) 5681–5686]. Our objective is to achieve higher structural transition temperatures than those of PMN–PT ceramics with as good dielectric, piezoelectric and electromechanical properties. Ceramics capacitance and loss tangent are measured when the ac field of measurement increases up to  $E = 0.5$  kV/mm. Behaviours of these materials under ac field are related to their coercive field and Curie temperature.  
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**Keywords:** Piezoelectric ceramic; PIN; PMN; PT; Non linear properties

### 19 1. Introduction

Complex perovskite so called relaxor  $\text{Pb}(\text{B}_1\text{B}_2)\text{O}_3$  ( $\text{B}_1 = \text{Mg, In, Sc...Yb}$ ;  $\text{B}_2 = \text{Nb, ...}$ ) (PMN, PIN, PSN) and  $\text{PbTiO}_3$  (PT) show high piezoelectric properties especially for compositions near the morphotropic phase boundary (MPB) [1–3]. Such complex perovskites are of greater interest for electronic ceramic devices, piezoelectric actuators, underwater and medical acoustic transducers. Single crystals [4] and ceramics [5] of PIN–PT, PIN–PMN–PT were investigated. Phase transitions of PIN–PT system were established by temperature dependence of dielectric constant [6] and X ray diffraction [7]. It has been reported that the PIN–PT system has a MPB zone near  $x = 37$ , which separates a rhombohedral zone for low PT concentrations from a tetragonal zone for high PT concentrations [7]. The PIN–37PT composition, showing two structural transitions at  $T_{\text{MT}} = 140$  °C between two ferro-

electric phases and at  $T_{\text{C}} = 300$  °C, exhibits good properties:  $P_{\text{r}} = 0.344$  C/m<sup>2</sup>,  $\epsilon_{33}^T$  (@1 kHz) = 2670,  $k_{\text{p}} = 57\%$  and  $k_{\text{t}} = 47\%$ .

This paper reports a study of PIN–PT and PIN–PMN–PT ceramics and compares their properties with those of PMN–33PT composition [8] which has a lower Curie temperature. Remanent polarisation, coercive field, piezoelectric constants and non linear dielectric properties under high ac electric field were measured and then compared with those of PMN–PT and PZT ceramics [9,10].

### 2. Ceramics by conventional sintering & hot forging

PIN–PT, PIN–PMN–PT ceramics were synthesised by two steps solid state reaction via Wolframite and Columbite phases. The Wolframite ( $\text{InNbO}_4$ ) or Columbite ( $\text{MgNbO}_4$ ) was formed by  $\text{In}_2\text{O}_3$  or  $\text{Mg}_2\text{O}_3$  with  $\text{Nb}_2\text{O}_5$  at 1100 °C for 24 h. The intermediate oxides were then mixed with  $\text{PbO}$  and  $\text{TiO}_2$  and ball-milled with Zirconium micro bead ( $\sigma < 1.6$  mm) using continuous attrition milling setup (Labstar). The mixtures were dried and calcined at 54

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55 850 °C for 2 h to form stoichiometric perovskites. The ultra  
 56 fine perovskite powder, showing the submicronic grain size  
 57 (Fig. 1a;  $\sigma \sim 0.2 \mu\text{m}$ ), was obtained by re-milling. The  
 58 green ceramics pellets with density about 50–60% of theo-  
 59 retic density were obtained by axial pressing. The green  
 60 PIN–PT pellets were hot-forged at 1000 °C for 1 h under  
 61 a pressure of 1 T/cm<sup>2</sup>. The hot-forged ceramics were finally  
 62 annealed under an O<sub>2</sub> flow at 1200 °C for 4 h. Yellow pale  
 63 translucent ceramics with high relative densities (>98%  
 64  $d_{\text{theoretical}}$ ) were achieved (Fig. 1b). Translucent PIN–PT  
 65 ceramics show large ceramic grain size over ten microns  
 66 and fine grain size about 1–2  $\mu\text{m}$  (Fig. 1c). Dense ternary  
 67 PIN–PMN–PT ceramics (>98%  $d_{\text{theo}}$ ), obtained using con-  
 68 ventional sintering, show fine and uniform grain size about  
 69 2  $\mu\text{m}$ . XRD spectra of both powder and ceramic show only  
 70 a single-phase perovskite.

### 71 3. Electromechanical properties

72 Samples were cut in discs (10 mm  $\times$  0.5 mm), plates  
 73 (10  $\times$  2  $\times$  0.5 mm<sup>3</sup>) and bars (10  $\times$  2  $\times$  1.5 mm<sup>3</sup>). Silver paste

74 was painted on the polished faces and fired at 700 °C dur-  
 75 ing 30 min.

76 PIN–PT samples were poled in a silicon oil under a  
 77 4000 V/mm field at room temperature during 10 min  
 78 whereas ternary PIN–PMN–PT and PMN–PT samples  
 79 were poled under a 400 V/mm field at 200 °C and then  
 80 cooled down to 50 °C under the same field. The tempera-  
 81 ture dependence of the dielectric constant was measured  
 82 at 1 kHz using a HP 4192A impedance analyser. Hysteresis  
 83 loops measurements were made using a Tower-Sawyer set-  
 84 up using triangle burst waves at 0.1 Hz. Electromechanical  
 85 properties were measured according to the IRE standard  
 86 method with an Agilent 4294A impedance analyser.

87 Table 1 resumes all the electromechanical constants at  
 88 low level (0.5 V) for the compositions  $x\text{PIN}-y\text{PMN}-z\text{PT}$ ,  
 89 PIN–37PT and PMN– $x\text{PT}$  [8]. Fig. 2 presents the temper-  
 90 ature dependence of the dielectric constant ( $\epsilon_{33}^T/\epsilon_0$ ) and the  
 91 radial coupling coefficient ( $k_p$ ) for PIN–37PT, PMN–33PT,  
 92 PMN–36PT and the two studied ternary compositions.

93 The dielectric curves, obtained at 1 kHz, present max-  
 94 ima at  $T_{\text{max}}$  (Fig. 2a) corresponding to the well known

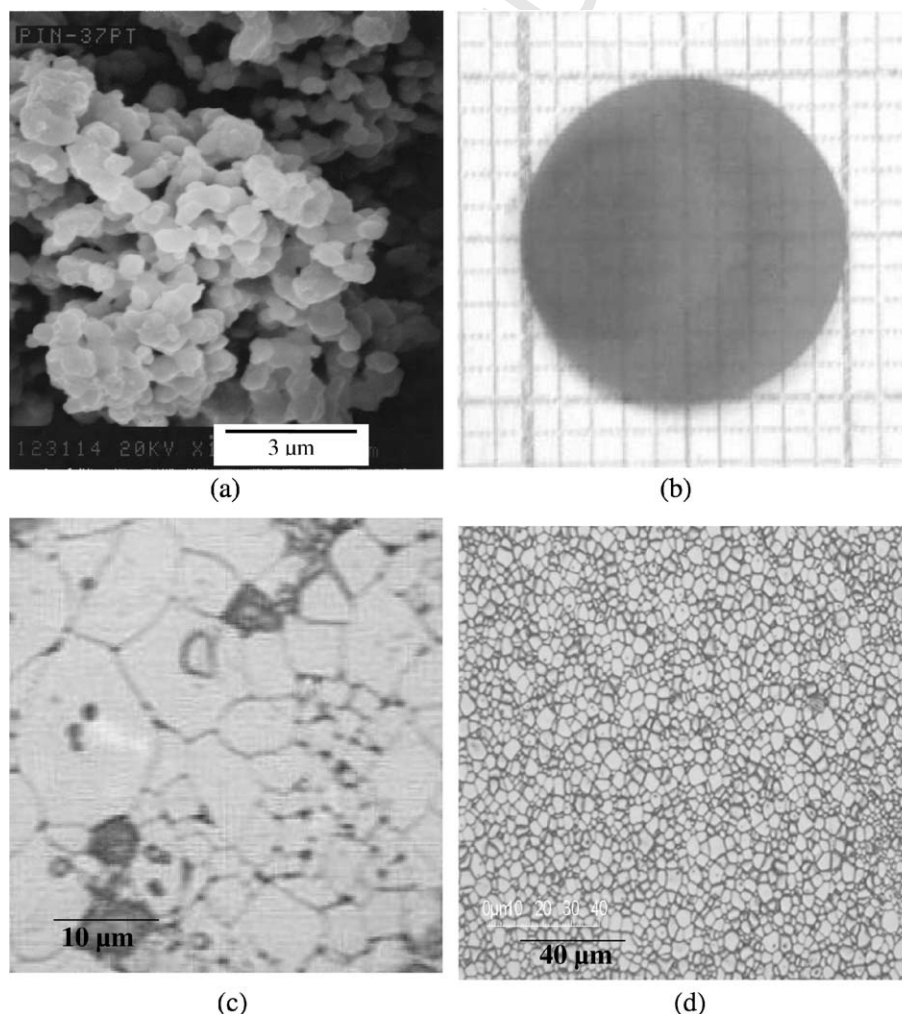


Fig. 1. Photographies of PIN–PT perovskite powder (a), PIN–PT translucent ceramic (b), microstructure of PIN–PT (c) and PIN–PMN–PT (d) ceramics.

Table 1

Dielectric and electromechanical properties of PIN–PMN–PT, PIN–PT and PMN–PT [8] ceramics

Properties	PIN–37PT	16PIN–51PMN–33PT	24PIN–42PMN–34PT	PMN–33PT	PMN–36PT
$\epsilon_{33}^T/\epsilon_0@1\text{kHz}$	2672	2420	3100	2920	4830
$k_{33}$	0.623	0.71	0.72	0.69	0.63
$d_{33}$ (pC/N)	428	416	496	453	499
$d_{33}$ Berlincourt (pC/N)	413	*	*	*	*
$s_{33}^E$ (pm <sup>2</sup> /N)	15	16	17	16	15
$M_{33} = (d_{33}/s_{33}^E)^2$ (C <sup>2</sup> /m <sup>4</sup> )	812	676	841	784	1089
$d_{33}\epsilon_0/\epsilon_{33}^T$ (pC/N)	0.160	0.172	0.16	0.155	0.103
$Q_m$	53	90	74	124	121
$k_{31}$	0.36	0.35	0.41	0.34	0.29
$d_{31}$ (pC/N)	–193	–189	–230	–186	–217
$s_{11}^E$ (pm <sup>2</sup> /N)	14	11	12	12	14
$Q_m$	76	110	91	*	*
$k_p$	0.57	0.62	0.61	0.58	0.52
$Q_m$	71	90	105	*	*
$k_t$	0.47	0.50	0.48	0.50	0.42
$Q_m$	71	100	140	*	*
$\epsilon_{11}^T/\epsilon_0@1\text{kHz}$	1716	2350	2500	2311	3105
$k_{15}$	0.51	0.53	0.52	0.40	0.50
$d_{15}$ (pC/N)	368	455	468	276	470
$s_{55}^E$ (pm <sup>2</sup> /N)	34	49	36	30	37
$Q_m$	41	60	60	*	*

95 tetragonal-cubic phase transition. As expected,  $T_{\max}$   
 96 increases from 175 to 180 °C, 195 and 290 °C, respectively  
 97 for PMN–33PT, ternary and PIN–37PT [7] compositions,  
 98 i.e., for the ceramics with increasing PIN concentration.  
 99 The dielectric curves present another anomaly due to the  
 100 rhombohedral–tetragonal or monoclinic–tetragonal phase  
 101 transition. This ferroelectric–ferroelectric transition takes  
 102 place towards 90 °C for the 24PIN–42PMN–34PT and  
 103 120 °C for 16PIN–51PMN–33PT. This anomaly is less  
 104 marked for PIN–37PT and is observed towards 80 °C for  
 105 the PMN–33PT.

106 PMN–36PT and PIN–37PT ceramics exhibit nearly the  
 107 same radial coupling coefficient at RT (Fig. 2b). PMN–  
 108 36PT ceramics show a decrease of the coupling coefficient  
 109 from RT ( $k_p = 0.55$ ) to 60 °C, then a continuous decrease  
 110 up to 160 °C ( $k_p = 0.38$ ) and a drop at 185 °C. This behav-  
 111 iour is consistent with the observed phase transitions of  
 112 PMN–36PT ceramics: ferroelectric–ferroelectric transition  
 113 around 80 °C and ferroelectric–paraelectric transition at  
 114 180 °C [4]. Ternary compositions exhibit a higher  $k_p$  at  
 115 RT that remains constant up to 85 °C, the temperature  
 116 of the ferroelectric–ferroelectric transition, then decreases  
 117 continuously up to 148 and 160 °C before dropping and  
 118 reaching plateau at 170 and 190 °C, respectively for  
 119 16PIN–51PMN–33PT and 24PIN–42PMN–34PT. It is  
 120 worth noting that PIN–37PT ceramics exhibit only slight  
 121 decrease of  $k_p$  from RT ( $k_p = 0.55$ ) up to 200 °C ( $k_p =$   
 122 0.41).

123 The electromechanical properties at low level (0.5 V) of  
 124 PIN–37PT are comparable with those of PMN–PT set  
 125 apart piezoelectric  $d_{ij}$  constants for which PMN–36PT pre-  
 126 sents much more important values. Among the two studied

ternary compositions, 24PIN–42PMN–34PT presents the  
 127 best dielectric and electromechanical properties (Table 1).  
 128 The dielectric constant at room temperature,  $\epsilon_{33}^T/\epsilon_0@$   
 129 1kHz = 3100, is intermediate between those of PIN–37PT  
 130 and PMN–36PT. The electromechanical properties of  
 131 ternary ceramics are comparable to those of PMN–PT  
 132 ceramics, the difference of dielectric constants being com-  
 133 pensated with the higher electromechanical coupling  
 134 coefficients.  
 135

#### 4. Non linear properties

136  
 137 Drift measurements or ac electric field dependences of  
 138 the dielectric constant were measured up to 1 kV/mm.  
 139 Sinusoidal signal at 1 kHz, generated from a HP 3314 A  
 140 function generator, was amplified by a Kepco Bipolar  
 141 Amplifier. A EG& G 5210 Lock-in Amplifier and an integra-  
 142 tion capacitance ( $C_i$ ) allow to measure the capacitance  
 143 ( $C$ ) at the sample connexions.

144 All materials show relatively square hysteresis loops  
 145 (Fig. 3). The coercive fields ( $E_c$ ) of ceramics containing  
 146 PIN are much higher than those in PMN–PT ceramics  
 147 (Table 2) and the remanent polarization ( $P_r$ ) is also higher:  
 148 this indicates a harder material than PMN–PT which is  
 149 consistent with the higher Curie temperatures.  $E_c$  and  $P_r$   
 150 increase with the increasing PT or PIN concentrations.  $E_c$   
 151 reaches 710 V/mm for PMN–36PT and 1660 V/mm for  
 152 PIN–37PT. At the same time,  $P_r$  reaches 0.344 C/m<sup>2</sup> for  
 153 PIN–37PT but 0.29 and 0.45 C/m<sup>2</sup>, respectively for  
 154 PMN–33PT and PMN–36PT. The two ternary composi-  
 155 tions present intermediate  $E_c$  and  $P_r$  between those of  
 156 PMN–PT and PIN–PT.

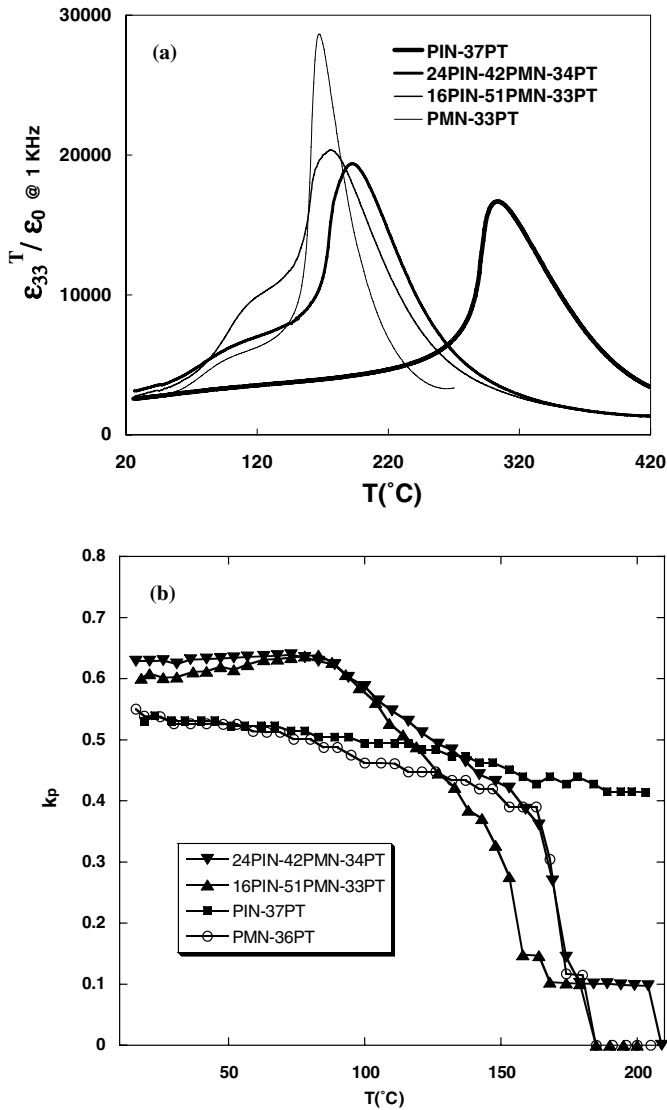


Fig. 2. Temperature dependence of the dielectric constant  $\epsilon_{33}^T/\epsilon_0@1\text{kHz}$  (a), and radial electromechanical coupling coefficient of PMN-PT, PIN-PT and PIN-PMN-PT ceramics (b).

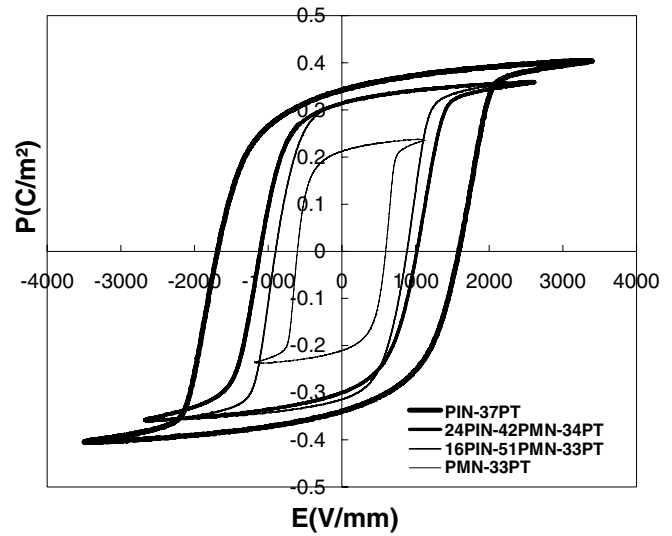


Fig. 3. Hysteresis loops of PMN-PT, PIN-PT and PIN-PMN-PT ceramics.

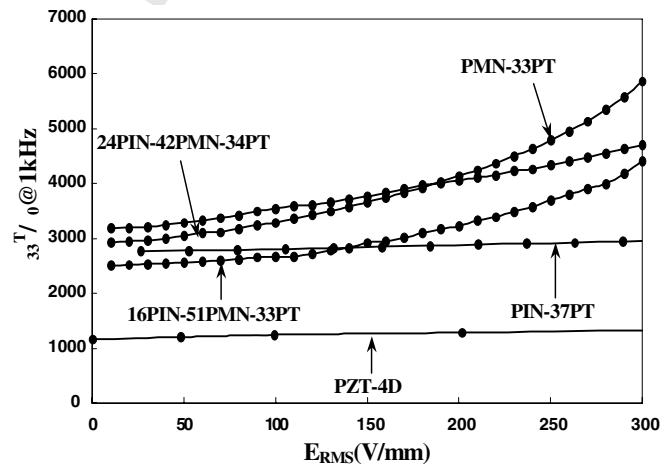


Fig. 4. Ac electric field dependence of the dielectric constant  $\epsilon_{33}^T/\epsilon_0@1\text{kHz}$  for different poled ceramics.

157 The ac electric field dependence of the dielectric constant  
158  $\epsilon_{33}^T/\epsilon_0@1\text{kHz}$  for poled ceramics are reported in Fig. 4. All  
159 ceramics present linear drift: the dielectric permittivity  
160  $\epsilon_{33}^T/\epsilon_0$  increases linearly with the ac applied electric field  
161 ( $E_{ac}$ ). It is related to some motions of the ferroelectric  
162 domain walls under the electric field. This is generally  
163 known as the “extrinsic contribution”. This linear drift is  
164 observed up to 300 V/mm for PIN-37PT and typical hard  
165 PZT-4D material while 24PIN-42PMN-34PT, 16PIN-

551PMN-33PT and PMN-33PT exhibit linear drift up to 166  
250, 150 and 120 V/mm. Above those fields, the latter 167  
ceramics show an accelerated drift behaviour: the permittivity 168  
increases very abruptly with the applied electric field. 169  
This thermal runaway phenomenon due to the increase of 170  
dielectric losses is in agreement with the observed low  $T_C$ . 171  
The higher the Curie temperature is, the higher is the 172  
required electric field to switch the polarization between 173  
adjacent ferroelectric domains. Therefore, the linear-drift 174

Table 2  
Curie temperature, coercive field and remanent polarisation of PMN-PT, PIN-PT and PIN-PMN-PT ceramics

	PMN-33PT	PMN-36PT	16PIN-51PMN-33PT	24PIN-42PMN-34PT	PIN-37PT
$T_C$ (°C)	160	180	180	195	300
$E_C$ (V/mm)	580	710	890	1020	1660
$P_r$ (C/m <sup>2</sup> )	0.29	0.450	0.316	0.314	0.344

175 region for PIN–37PT and PZT–4D is larger than that for  
176 ceramics containing PMN, and the accelerated drift region  
177 is not observed.

178 The linear drift can be characterized by the Rayleigh  
179 coefficient:  $\alpha_{ac}^T = \frac{1}{\varepsilon_{330}^T} \left( \frac{\partial \varepsilon_{33}^T}{\partial E_{ac}} \right)$ . As expected, the Rayleigh coef-  
180 ficients of PIN–37PT and PZT–4D have the same value,  
181  $\alpha = 3.4$ , and increases to 17.2, 27.4 and 33.4 for ternary  
182 and PMN–33PT ceramics.

## 183 5. Conclusions

184 Among PIN–*x*PT compositions, PIN–37PT presents the  
185 best dielectric and electromechanical properties at low level  
186 [5]. Such a behaviour is characteristic of morphotropic  
187 compositions. The important values of  $\varepsilon_{ij}^T$ ,  $s_{ij}^E$ ,  $d_{ij}$  and the  
188 low  $Q_m$  values of PIN–37PT are characteristic of a soft  
189 material.

190 The electromechanical properties of PIN–37PT are com-  
191 parable to those of PMN–PT except lower dielectric and  
192 piezoelectric  $d_{ij}$  constants. The dielectric constant at room  
193 temperature is directly related to the Curie temperature:  
194 generally, the more the Curie temperature is raised, the  
195 lower is the dielectric constant at room temperature.  
196 PIN–37PT presents a Curie temperature  $T_C = 300^\circ\text{C}$   
197 higher than that of PMN–36PT,  $T_C = 180^\circ\text{C}$ . Its dielectric  
198 constant and thus its piezoelectric constants at room tem-  
199 perature are lower than those of PMN–36PT. The incorpo-  
200 ration of PIN in PMN–PT ceramics results in an increase  
201 of structural transition temperatures and thus a decrease  
202 of the dielectric constant at room temperature.

203 The electromechanical properties of ternary ceramics  
204 are similar to those of PMN–PT ceramics, the difference  
205 between dielectric constants being compensated by the  
206 higher electromechanical coupling coefficients.

207 The temperature dependence of the planar electrome-  
208 chanical coupling coefficient shows that the higher the  
209 Curie temperature is, the better is the stability of  $k$ . There-  
210 fore, the higher the ferroelectric–ferroelectric temperature  
211 transition is, the more the decrease of  $k$  is delayed. These  
212 same tendency should be observed for the other electrome-  
213 chanical constants.

214 Our purpose is thus to synthesise materials having struc-  
215 tural transition temperatures high enough to delay the drop  
216 of the electromechanical properties when temperature is  
217 increased. However, power applications require high  
218 dielectric and piezoelectric constants. From this point of  
219 view, PIN–PMN–PT ceramics seem to be a good  
220 candidate.

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